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APOLLO SOYUZ TEST PROJECT G&N ERROR ANALYSIS (CM 111/IMU 25)

by

S. B. Helfant

June 1975





The Charles Stark Draper Laboratory, Inc.

Cambridge, Massachusetts 02139

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Approved:

N. Sears

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ACKNOWLEDGMENT

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This volume is the combined effort of the following additional people: Linda Willy prepared the component performance tabulation and performed the plotting for the inertial components. William Beaton provided the failure rates for the success probability. Their contribution to the preparation of this volume is greatly appreciated.

The publication of this report does not constitute approval by the National Aeronautics and Space Administration of the findings or the conclusions contained herein. It is published only for the exchange and stimulation of ideas.

 $V(x,y) = \left(\frac{1}{2} \left(\frac{1}{2} \left(\frac{y}{x} \right) \right) + \frac{1}{2} \left(\frac{y}{x} \right) \right) + \frac{1}{2} \left(\frac{y}{x} \right) +$

ABSTRACT

This document presents data on G&N system performance and operation for the CM. For data on the effects of Block II and of measured CM IMU test data deviation uncertainties on earth orbit insertion indication uncertainties and on deorbit burn and reentry uncertainties, the reader is referred to E-2760, the G&N error analysis report for Skylab 2).

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GYRO DRIFT TEST POSITIONS FOR SUNDANCE, LUMINARY, COLOSSUS, AND ON

STABLE MEMBER POSITION	STABLE MEMBER ORIENTATION	HORIZONTAL DRIFT	VERTICAL DRIFT
1	X DOWN Y SOUTH Z WEST	NBDY-ADOAY	
2	X DOWN Y WEST Z NORTH	+NBDZ-ADOAZ	-NBDZ+ADIAX
3	X SOUTH Y WEST Z DOWN	NBDX-ADOAX	
4	X EAST Y SOUTH Z DOWN	+NBDY+ADSRAY	+NBDZ+ADIAZ
5*	X WEST Y UP Z NORTH	+NBDZ-ADSRAZ	
6*	X SOUTH Y DOWN Z EAST	+NBDX+ADSRAX	-NBDY+ADIAY
7	X NORTH Y UP-WEST Z UP-EAST	-NBDX+(ADSRAX/√2)	
8	X EAST Y UP-NORTH Z UP-SOUTH	$(-NBDZ-NBDY)/\sqrt{2}$ +(ADIAZ-ADIAY)/2 +(ADSRAY+ADSRAZ)/2	
9	X UP-EAST Y UP-WEST Z SOUTH	-NBDZ+(ADSRAZ/√2)	
10	X UP-NORTH Y UP-SOUTH Z EAST	$(NBDY-NBDX)/\sqrt{2} + (ADIAY-ADIAX)/2 + ADSRAX/2$	
11	X NORTH Y WEST Z UP	-NBDX-ADOAX	
12	X UP Y SOUTH Z EAST	+NBDY+ADOAY	
13	X UP Y EAST Z NORTH	+NBDZ+ADOAZ	

^{*}Positions 5 and 6 are lab test only.

G&N MISSION RELIABILITY ANALYSIS

Failure rates used were obtained, for the most part, from observed Apollo field and flight experience of the PGNS. Each reported failure was analyzed with respect to its likelihood of occurrence in flight and the impact on the Mission should such failure occur. The result was to count only those reported failures which could occur in flight and which would degrade the Mission, should they occur.

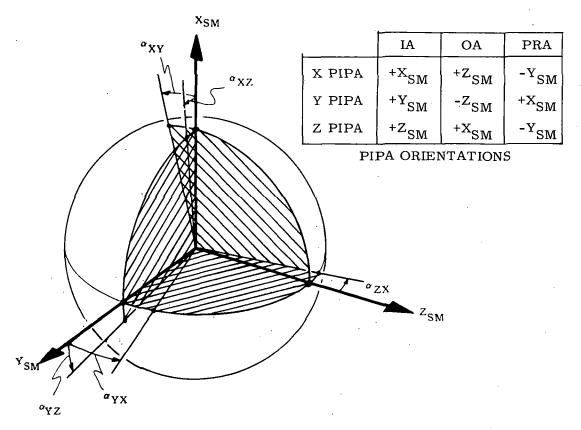
SUBSYSTEM	MODE (time/cycles)	FAILURE RATE ($\lambda \times 10^6$)	MISSION DURATION (hrs or cycles)	e - λt
AGC	Operate	19.2	218	0.99582
	Calendar	2.8	218	0.99939
	Envirn	30.9	0.2	0.99999
	On/Off	238.1	0	1.00000
DSKY*	Operate	1.4	218	0.99999
	Calendar	0.9	218	0.99999
	Envirn,	122.9	0.2	0.99999
	On/Off	1190.5	0	1.00000
IMU CDU**	Operate	20.2	218	0.99561
	Calendar	2.4	218	0.99948
	Envirn	62.5	0.2	0.99999
	On/ O ff	1666.6	0	1.00000
IMU	Operate	94.1	218	0.97969
	Calendar	2.6	218	0.99943
	Envirn	18.5	0.2	0.99999
	On/Off	142.9	0	1.00000
IMU Electronics (PSA)	Operate Calendar Envirn On/Off	8.4 1.2 18.5 714.3	218 218 0.2 0	0.99817 0.99974 0.99999 1.00000
Optics Assembly	Operate	119.3	218	0.97433
	Calendar	1.8	218	0.99961
	Envirn	18.5	0.2	0.99999
	On/Off	238.1	0	1.00000
Optics Electronics	Operate	17.2	218	0.99626
	Calendar	7.1	218	0.99845
	Envirn	18.5	0.2	0.99999
	On/ O ff	142.9	0	1.00000

G&N MISSION RELIABILITY

CM = 0.93736

^{*}Considers parallel redundancy (1-(1-e^{-\lambda t})²)

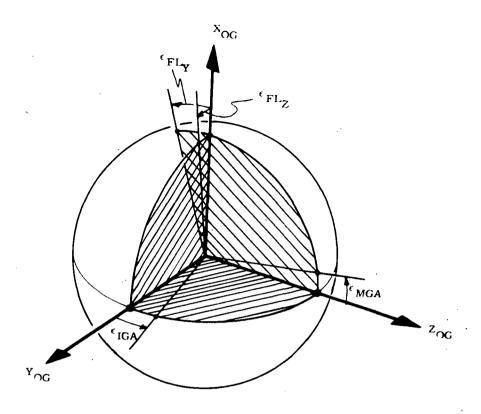
^{**}Includes CM Optics CDU



PIPA Misalignments from Ideal Stable Member Axes

	(Angle in Sec)
Term	CM-IMU 25
$\alpha_{\rm XY}$	+ 24
$\alpha_{ m XZ}$	+ 7
$\alpha_{ m YZ}$	+ 6
$\alpha_{ m YX}$	- 14
$^{lpha}_{ m ZX}$	+ 3

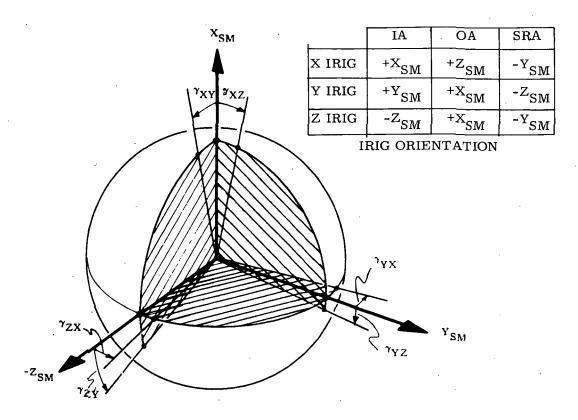
DEFINITION OF POSITIVE SENSE
PIPA INPUT-AXIS MISALIGNMENTS
with respect to
IDEAL STABLE MEMBER AXES



Gimbal Axis Orthogonality Errors and Outer Gimbal Misalignment from Casemounting Axes

×	(Angle in Sec)
Term	CM-IMU 25
$\epsilon_{ m IGA}$	+ 6
$\epsilon_{ ext{MGA}}$	- 20
$\epsilon_{ ext{FLY}}$	- 1
$\epsilon_{ ext{FLZ}}$	- 9

DEFINITION OF POSITIVE SENSE
GIMBAL AXIS ORTHOGONALITY
and
OUTER GIMBAL ALIGNMENT
with respect to
CASE MOUNTING ALIGNMENT



IRIG Misalignments from Ideal Stable Member Axes

	(Angle in Sec)
Term	CM-IMU 25
$^{\prime}_{ m XY}$	- 46
XZ	+ 2
YZ	+ 50
$^{ u}_{ m YX}$	+ 106
ZX	- 145
^р ZY	+ 16

Block II G&N
DEFINITION OF POSITIVE SENSE
IRIG INPUT-AXIS MISALIGNMENTS
with respect to
IDEAL STABLE MEMBER AXES

IMU S/N 25 CM 111/G&N 215

 IRIGs
 PIPAs

 X = 8A128 X = 2AP110R

 Y = 8A121 Y = 2AP276

 Z = 8A120 Z = 2AP282

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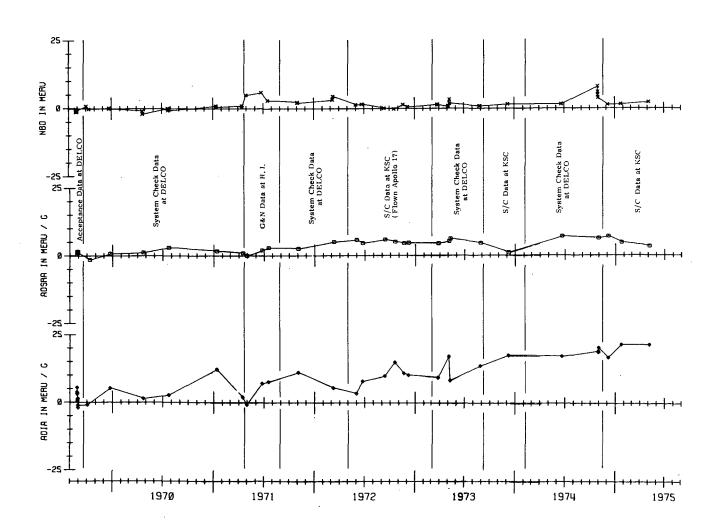
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	ADSRA			p. 9		KSC		7.1	8.4	3.4								
	NBD	8.1	6.3	6.3	3.8	DELCO TO	CM-111	1.3	٠.	2.3								
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	LOC	SB6	SB6	SB6	SB6	IMU	IMU	KOB	KOB	K91								
-	DATE	300C74	300074	300C74	310074	18N074	26 NO 74	5DE74	22JA75	5MX75	78Y75							

G&N 215, CM 111, IMU 25, APOLLO IRIG 8A128, X AXIS



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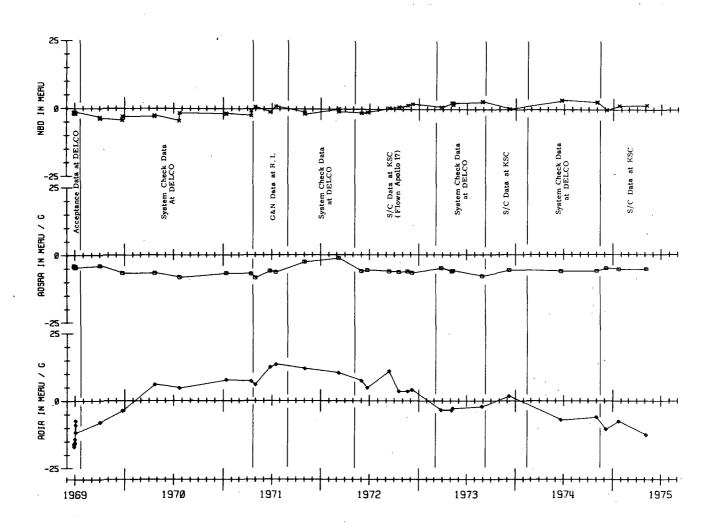
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10.0 GEN 21M TESTALLED TS C**-11M. 10.0 GEN X 20 21M - 0.7	TST IMU GEN TYP ASSN SYS	ADSRA	ADIA	DELSP+, DELSP	WHE-	+I SEUCH	1- ro	A DOA
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0. SHIPED POOR NR TO DELCK/MER. 11.9 3) SPO X 20 3) SPO X 20 4.13 SPO X 20 5) SPO X 20 5) SPO X 20 6. 1.9 6. 1.9 7. 1.	SC GEN X 20 218 -		12.5	384	340			
13 SPO X 20 14 SPO X 20 15 SPO X 20 17 SPO X 20 18 SPO X 20 18 SPO X 20 19 SPO X 20 19 SPO X 20 10 SP	SC GEN X 20 0.9	π.9 -	13.5		381			
35 PO X 20	MU 20 SHIPPED FPOM NR TO N3 SPO V 20	DELCOZEKE.	11 0					
13 SPO X 20 14 SPO X 20 15 SPO X 20 16 SPO X 20 17 SPO X 20 18 SPO X 20 18 SPO X 20 19 SPO X 20 10 SPO	03 SPO X 20 -	2.	•					6.7
1569 2500 X 20 20 C.1 1.2 10.3 17 361 26 EVILD PRANKIENT OBSERVED DIBING GRAVITY PRANSIENT TEST. 10-70 SHIPPED FROM DISCOVARF TO KS2 10-70 INSTRALEDS IN CA-114 AF KS2. 10-70 INSTRALED IN CA-114 AF KS3. 10-70 INSTRALED I	03 SPO X 20				227	84.99		
0.3 SEO X 20 0. 1.0 0. 1.1.2 0. 1.1.2 0. 1.1.0 0						1569		
0.3 SERVED PRANSIENT OBSERVED DUE 11.2 0.2 SERVED PRANSIENT OBSERVED DUE 11.2 0.4 - 1.5 - 1.4 0.5 SERVED PROM DELCO-MENT TO KSZ 0.7 - 1.4 - 6.2 0.8 - 1.5 - 1.5 0.9 GEN X 20 218 0.9 - 6.2 1.0 - 2.3 0.9 GEN X 20 218 0.9 - 6.2 1.0 - 2.3 0.9 GEN X 20 218 0.9 - 6.2 1.0 - 6.2 1.0 - 2.3 1.0 - 1.5	03 SPO X 20		10.3	1			•	
### ### ### ### ### ### ### ### ### ##	03 SPO X 20	- 1.2			361	85.016		
## 19 Factor Fact	O FLOID TRANSLENT OF THE STATE	INDURING GO			EST.			
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0.00 GEN X 20 218	OB GEN X 20 218 -	}	7.4					3.1
94 GEN X 20 218	OB GEN X 20 218 -	7.5	6.11	150	7.5			3.2
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## CANTACA COLOR PROPERATION: NBD = 0.6. ADTA = 7.0 ANSRA = -6.0 ## CAN X 20 218	9A GEN X 20 218		•					2.0
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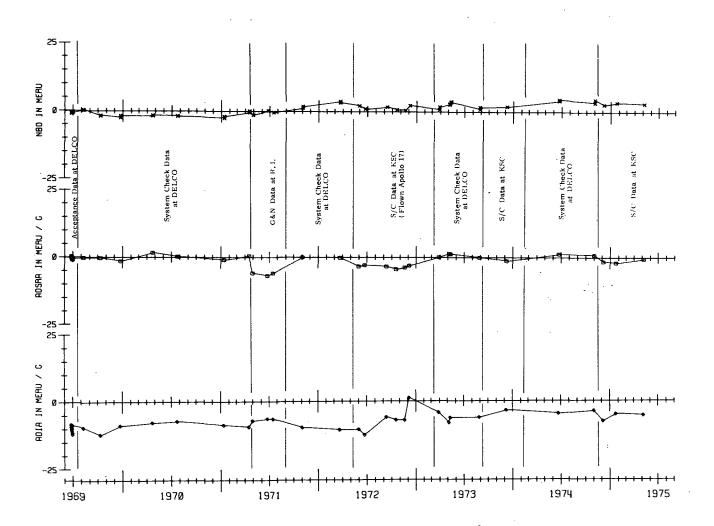
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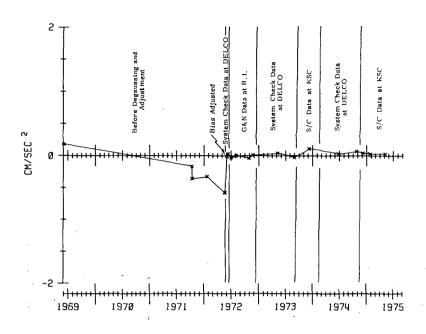
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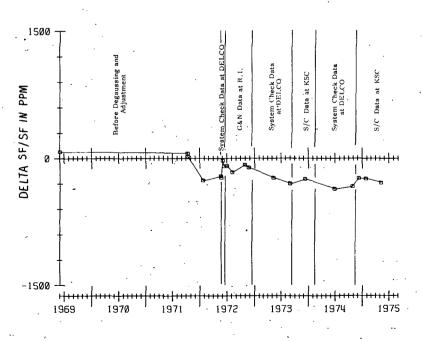
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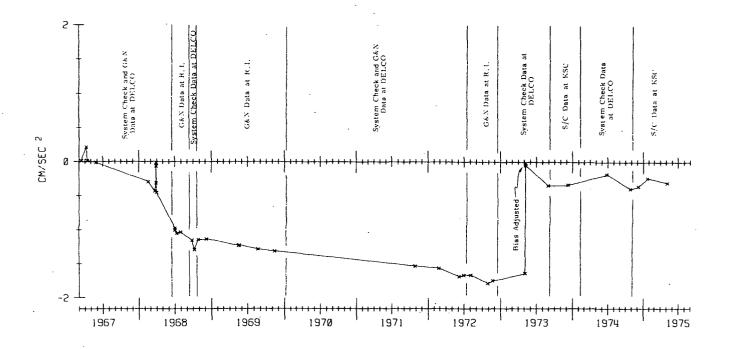
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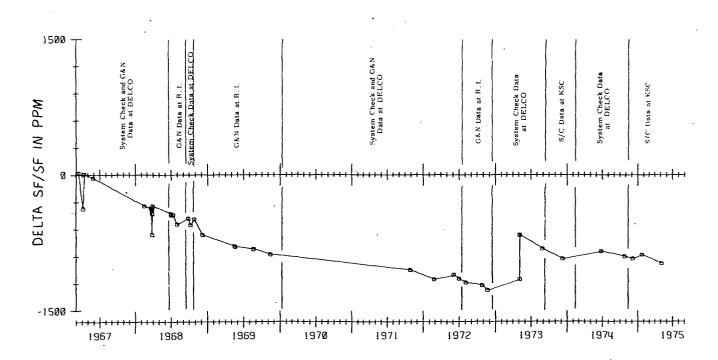
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	- 983	- 983	- 983		0	3				

G&N 215, CM 111, IMU 25, APOLLO PIPA 2AP276, Y AXIS



1-G BIAS DRIFT PLOTTED BY TIME



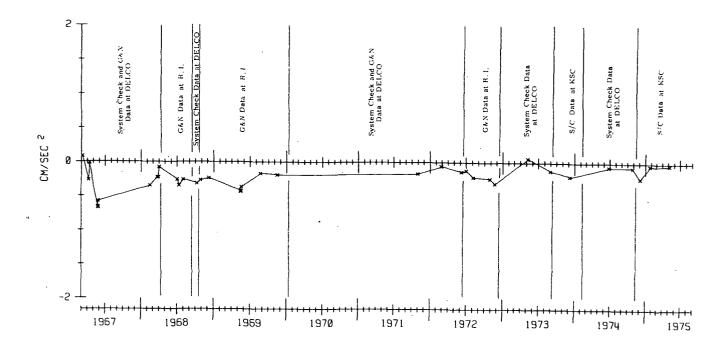
SCALE FACTOR DRIFT PLOTTED BY TIME

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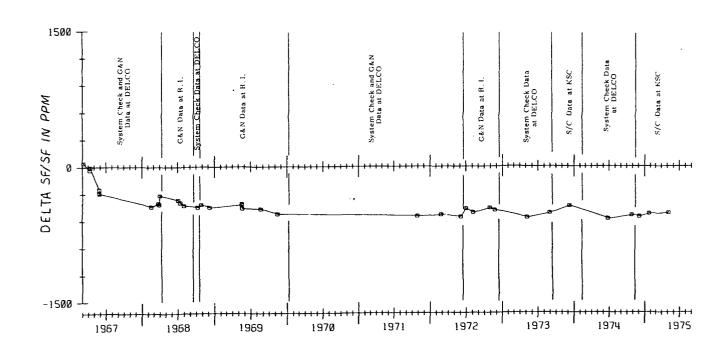
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150872	REMOVED	PPOH	CM-119	CM-119 AT NR.					
19 DE72	SHIPPED	FROM	CT 4M	DELCO.					
7H Y 7 3	SB5 SPO	2 25		- 569	9.06	0.10		0.05	103.6583
8 4773	SBS SAL	2 25				(0.07)	15		
28AU73	SB6 SPO			- 519	-0.12	-0.11			103,6621
29AU73	SB6 SAL	52 2				(-0.15)	r	9.04	
12SE73	IMU-25	MOVED	PROM	MOVED PROM DELCO TO KSC,	TO KSC,	SI-RESC	SI-RESCUE VEHICLE		
245873	IM3-25	INSTA	LLED	IN CM-1	19, GEN-	213, SL-P	INSTALLED IN CM-110, GEN-213, SL-PFSCUE VEHICL	a 1	
07DE73	N35 86X	52 2	213	- 440	-0.20				
13PE74	140 25	SHIPPED	MCdd (KSC TO PELCO				
25JE74		2 25		- 583	-0.06	-0.01		0.04	103.665(
28JE74		2 25				(-0.0H)	- 2		
2 50C 74	SB6 SPO	SPO 2 25		- 541	-0.07	-0.05		0.04	103.663
4 NO 74	SB6 SAL	52 2				(-0.02)	٣	•	
18NO7u	25	SHIPPED		PROM DELCT	TO KSC				
26N074	1MU 25	INSTAL	LED I	25 INSTALLED IN CH-111	_				
50874	KOB GEN	7 2	5 215 -		-0.23				
22JA75	KOB GEN	2 2	215	- 526	-0.0-				
D SMY75	KAB GEN	2 2	215	- 520	-0.03				

G&N 215, CM 111, IMU 25, APOLLO PIPA 2AP282, Z AXIS



1-G BIAS DRIFT PLOTTED BY TIME



SCALE FACTOR DRIFT PLOTTED BY TIME

STANDARD DEVIATION (10) OF THE IRIG AND PIPA PARAMETER UNCERTAINTIES USED FOR MISSION PERFORMANCE SUMMARY CM 111, IMU 25

PARAMETER			
IMU Axis	<u>X</u>	<u>Y</u>	· <u>Z</u>
PIPAs			
Data Compilation Period 12/05/74 - 5/05/75			
Accelerometer Bias (cm/sec ²)	0.01	0.06	0.11
Scale Factor (SF/SF ppm)	29	48	21
IRIGs			
Data Compilation Period 12/05/74 - 5/05/75			
Bias Drift (MERU)	0.5	0.9	0.4
ADSRA (MERU/g)	1.9	0.2	0.7
ADIA (MERU/g)	2.8	2.5	1.4
ADOA (MERU/g)	0.1	0.4	0.2

Data is based upon performance in the IMU. Point-to-point stability in operation is much better than the above data.

PROPOSED GYRO AND ACCELEROMETER PERFORMANCE COMPENSATIONS

PARAMETER			
IMU Axis	<u>X</u>	<u>Y</u>	<u>Z</u>
PIPAs			
Accelerometer Bias (cm/sec ²)	+0.03	-0.31	-0.03
Scale Factor (SF/SF ppm)	-290	-980	-520
IRIGs			
Bias Drift (MERU)	+0.7*	+1.6	+3.0
ADSRA (MERU/g)	+3	- 5	· -1
ADIA (MERU/g)	+22	-13	- 5

^{*}Compensation selected as NBD -ADOA

Dictionary of Terms

ACC Acceptance Test Data

ACD After Cooldown

ACE A.C. Electronics (presently Delco Electronics)

ADJ Adjusted

ADOA Acceleration Sensitive Drift Due to Acceleration along the OA

BCSW Binary Current Switch

BIA Bias Adjusted

BUSS High, Low, or Nominal Direct Current Test

CDN Post Cooldown

CQL Component Qualification
CRQ Component Regualification

CRR Retest after Minor Adjustment or Resistor Changes

CRT Retest Data

CSS Short Servo Test

CVR Component Verification

DGI Degaussed IRIG

DGS Degaussed

F/F Float Freedom
FST Final Stability

GAL Guidance & Navigation PIPA Alignment

G&N Guidance & Navigation System Measurement

GP Gaussed PIPAs HBS Hi Bus Voltage

I&A Inspection and AcceptanceISS Inertial Subsystem Data

KSC Kennedy Space Center

LBS Lo Bus Voltage

MW Milliwatt

NAR North American Rockwell (presently Rockwell International, Inc.)

NBS Nominal Bus Voltage

OOS Out of Spec

RDT Wheel Rundown Time, Seconds

RI Rockwell International

APPENDIX

ELECTRICAL POWER REQUIREMENTS

This section was extracted from the MIT/IL Report E-1142 (Rev. 59) "SYSTEM STATUS REPORT". It is included in this report for convenience.

Electrical power and energy reporting is based upon the inflight spacecraft sequence of events for the Design Reference Mission as developed by the Apollo Mission Planning Task Force (AMPTF). (Reference GAEC Report Volume III - LED-540-12, dated October 30, 1964).

The accompanying diagrams present the power drawn through the spacecraft circuit breakers. It is assumed that power is drawn from the spacecraft's primary +28VDC supply and a 400 cps-115 VAC single-phase inverter.

Intermittent power peaks can exist, particularly during operation of displays and controls at random times. The energy content in these peaks is considered negligible.

All values (except those mentioned above) are actual expected levels of power at 28.0 VDC. They are based on measured values on G&N systems 207 and 208 for the Block II Command Module. No margin factor has been applied to protect against possible differences between G&N systems and spacecrafts. Thus, these values should not be taken as "not to exceed" extremes.

The following Interface Control Documents serve as the guidelines for reporting power figures.

CM Block II MH01-01327-216 "G&N Electrical Input Power" signed 15 July 1965.

BLOCK II GUIDANCE & NAVIGATION LOAD ON PRIMARY +28 VDC COMMAND MODULE

BASED UPON 1985 MOURS (8.27 DAY) LUNAR ORBIT MISSION DESIGN REFERENCE MISSION

STATUS OCTOBER 1967

REFERENCE GAFC REPORT - LED 540-12, 30 OCTOBER 1964
APOLLO MISSION PLANNING TASK FORCE

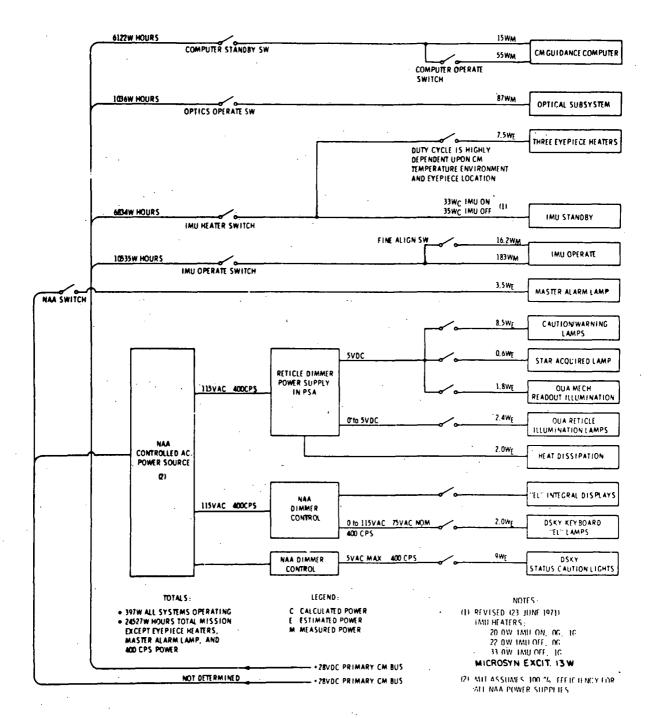


Figure A-1

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